

ECE 321C

Electronic Circuits

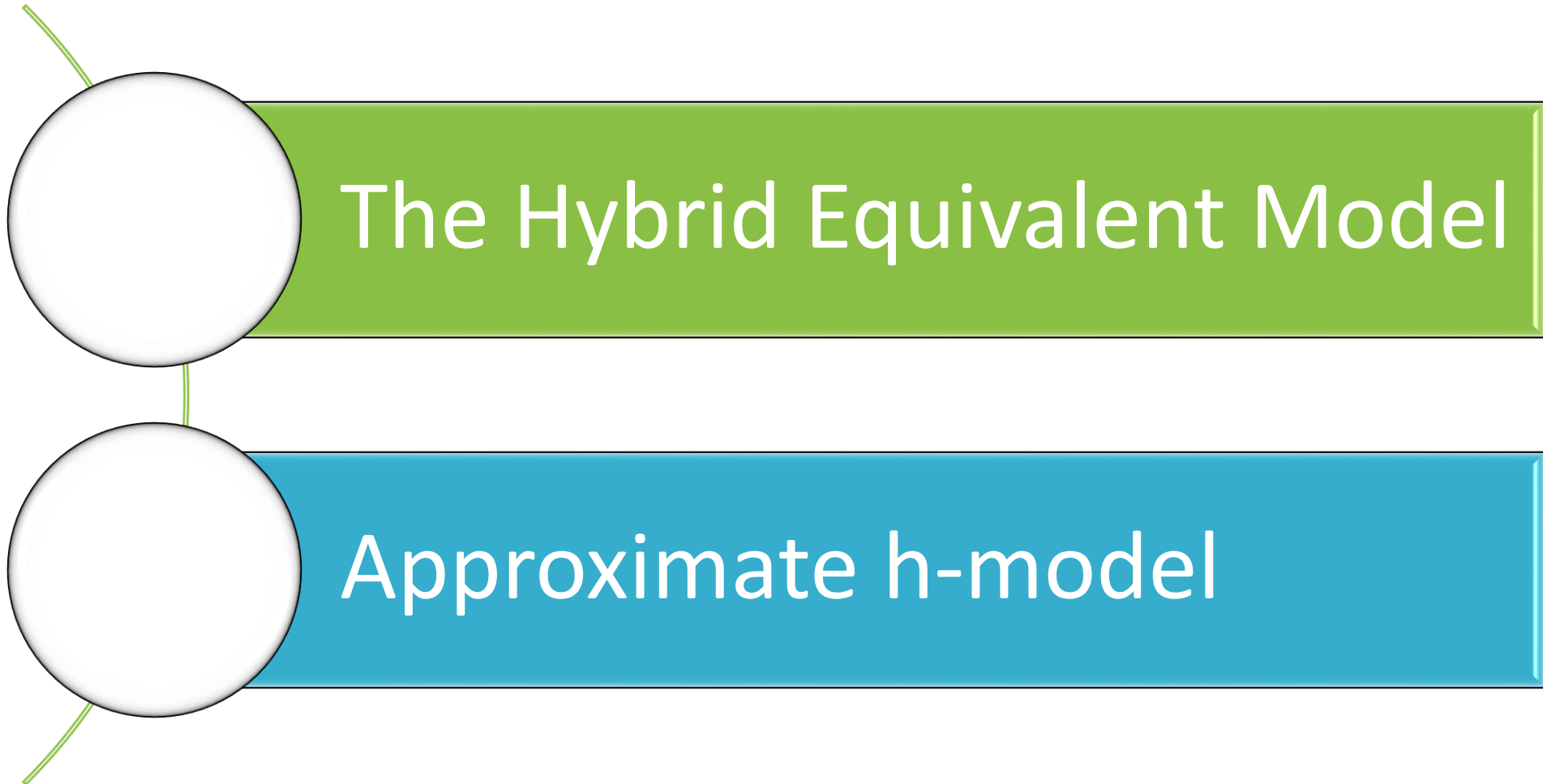
Lec. 5: BJT Modeling and re Transistor Model (Hybrid Equivalent Model) (2)

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Agenda



The Hybrid Equivalent Model

The Hybrid Equivalent Model

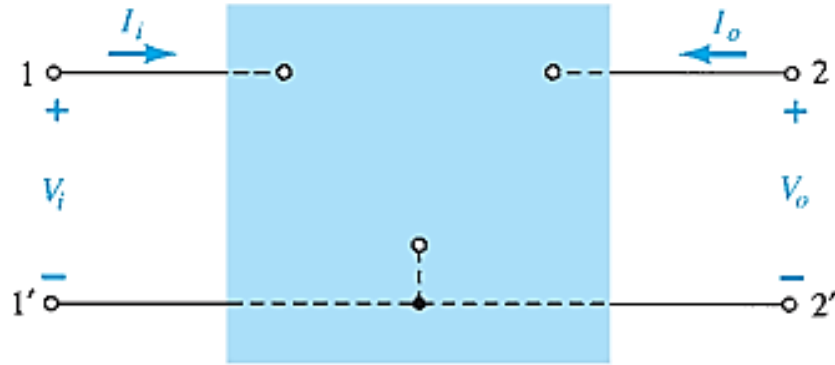
- Main Difference between r_e and H model is that:
 - The r_e model has the advantage that the parameters are defined by the actual operating conditions
 - The parameters of the hybrid equivalent circuit are defined in general terms for any operating conditions.

		Min.	Max.	
Input impedance ($I_C = 1 \text{ mA dc}$, $V_{CE} = 10 \text{ V dc}$, $f = 1 \text{ kHz}$)	h_{ie}	0.5	7.5	$\text{k}\Omega$
Voltage feedback ratio ($I_C = 1 \text{ mA dc}$, $V_{CE} = 10 \text{ V dc}$, $f = 1 \text{ kHz}$)	h_{re}	0.1	8.0	$\times 10^{-4}$
Small-signal current gain ($I_C = 1 \text{ mA dc}$, $V_{CE} = 10 \text{ V dc}$, $f = 1 \text{ kHz}$)	h_{fe}	20	250	—
Output admittance ($I_C = 1 \text{ mA dc}$, $V_{CE} = 10 \text{ V dc}$, $f = 1 \text{ kHz}$)	h_{oe}	1.0	30	$1 \mu\text{S}$

FIG. 5.92

Hybrid parameters for the 2N4400 transistor.

The Hybrid Equivalent Model



$$V_i = h_{11}I_i + h_{12}V_o$$

$$I_o = h_{21}I_i + h_{22}V_o$$

FIG. 5.93
Two-port system.

$$h_{11} = \left. \frac{V_i}{I_i} \right|_{V_o=0}$$

ohms → short-circuit input-impedance parameter

$$h_{21} = \left. \frac{I_o}{I_i} \right|_{V_o=0}$$

unitless → short-circuit forward transfer current ratio parameter

$$h_{12} = \left. \frac{V_i}{V_o} \right|_{I_i=0}$$

unitless → open-circuit reverse transfer voltage ratio parameter

$$h_{22} = \left. \frac{I_o}{V_o} \right|_{I_i=0}$$

siemens → open-circuit output admittance parameter

Transistor Hybrid Equivalent Circuit

- Hybrid Equivalent Circuit:

$$V_i = h_{11}I_i + h_{12}V_o$$

$$I_o = h_{21}I_i + h_{22}V_o$$

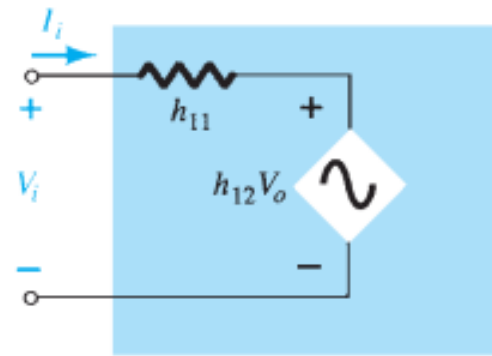


FIG. 5.94

Hybrid input equivalent circuit.

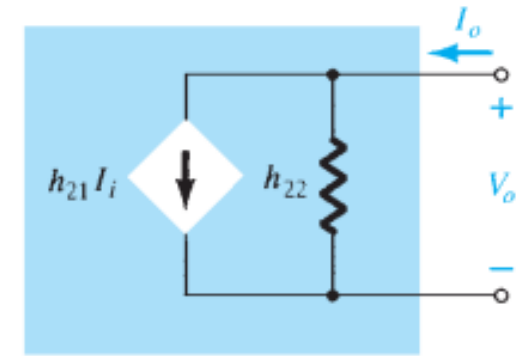


FIG. 5.95

Hybrid output equivalent circuit.

- For Transistor:

$h_{11} \rightarrow$ input resistance $\rightarrow h_i$

$h_{12} \rightarrow$ reverse transfer voltage ratio $\rightarrow h_r$

$h_{21} \rightarrow$ forward transfer current ratio $\rightarrow h_f$

$h_{22} \rightarrow$ output conductance $\rightarrow h_o$

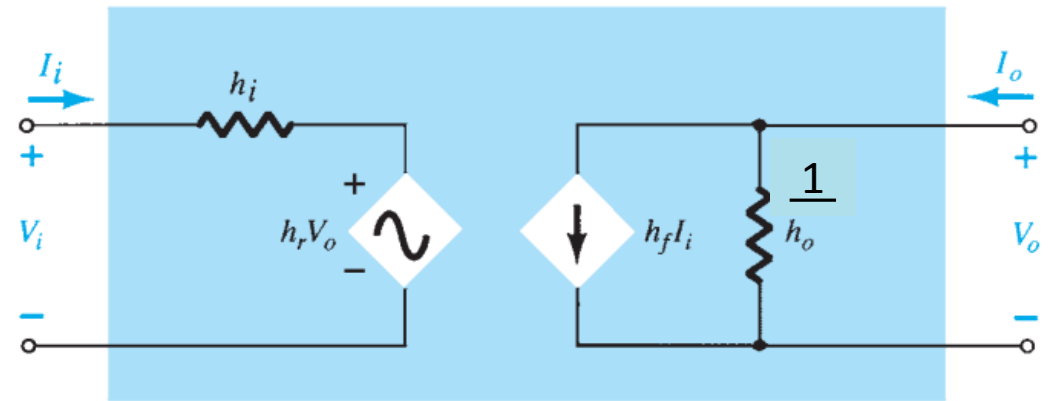


FIG. 5.96

Complete hybrid equivalent circuit.

Transistor Hybrid Equivalent Circuit (CE)

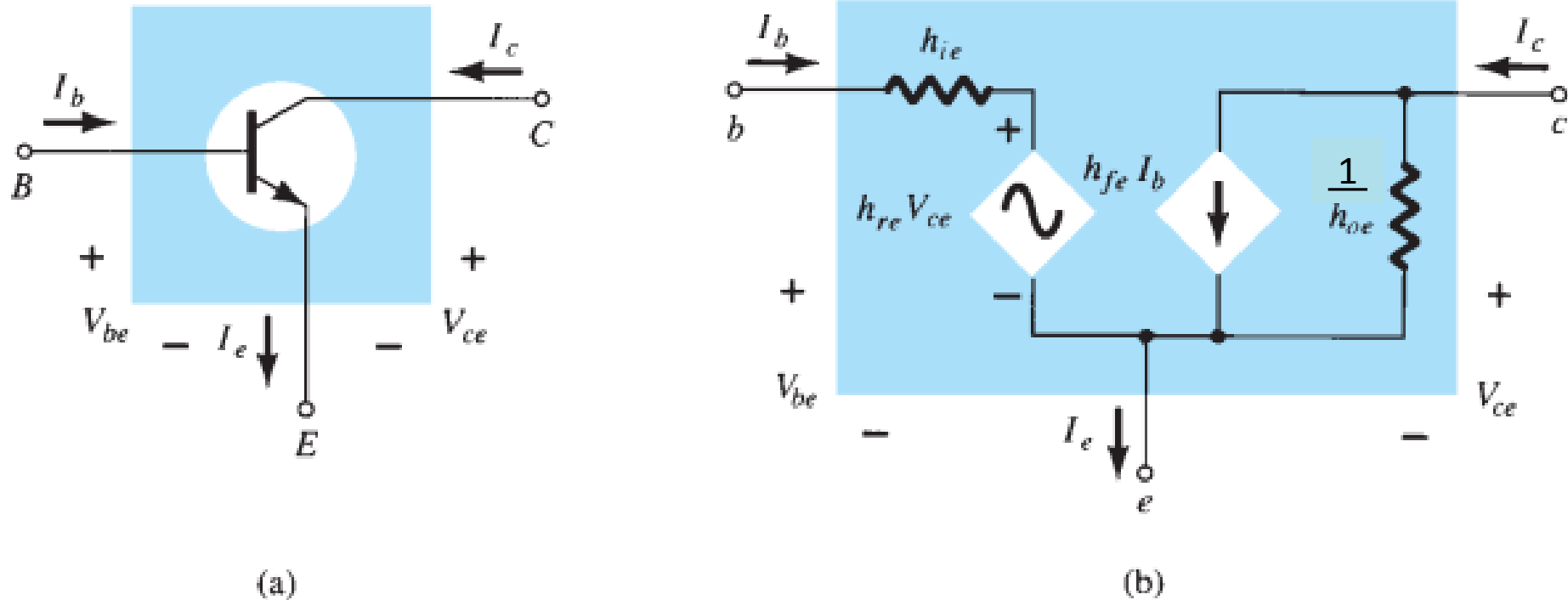


FIG. 5.97

Common-emitter configuration: (a) graphical symbol; (b) hybrid equivalent circuit.

Transistor Hybrid Equivalent Circuit (CB)

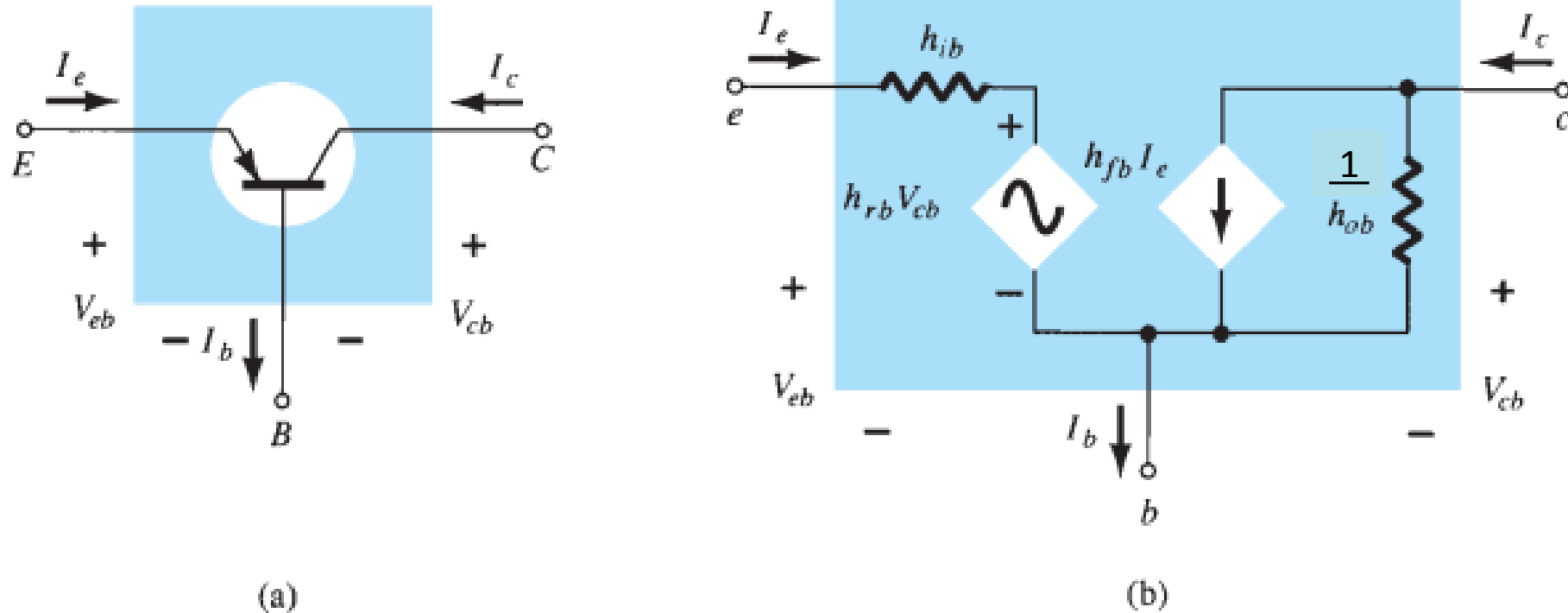


FIG. 5.98

Common-base configuration: (a) graphical symbol; (b) hybrid equivalent circuit.

Hybrid Approximation

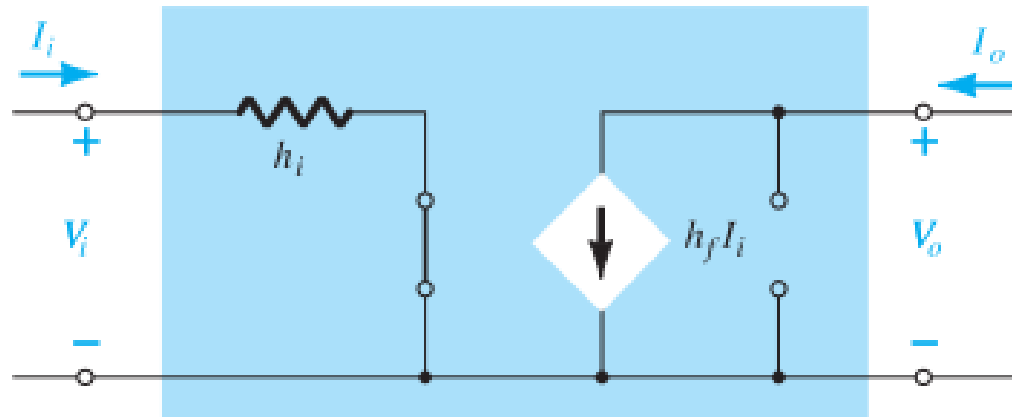


FIG. 5.99

Effect of removing h_{re} and h_{oe} from the hybrid equivalent circuit.

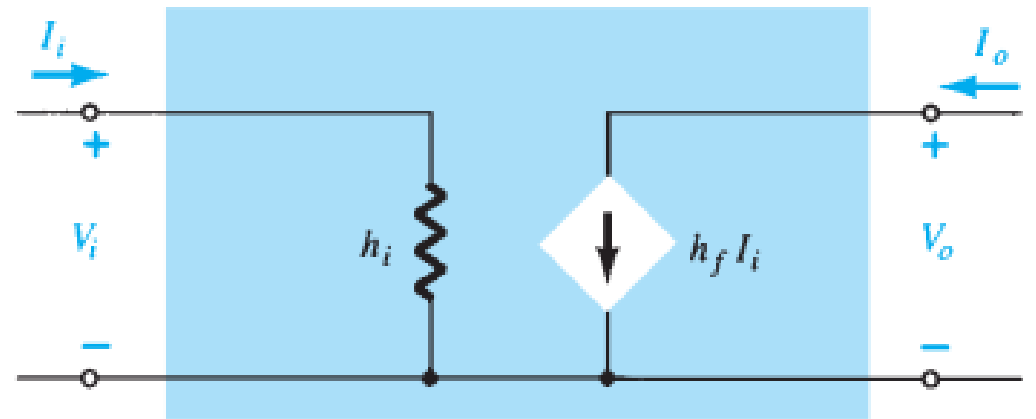


FIG. 5.100

Approximate hybrid equivalent model.

Hybrid vs. r_e model

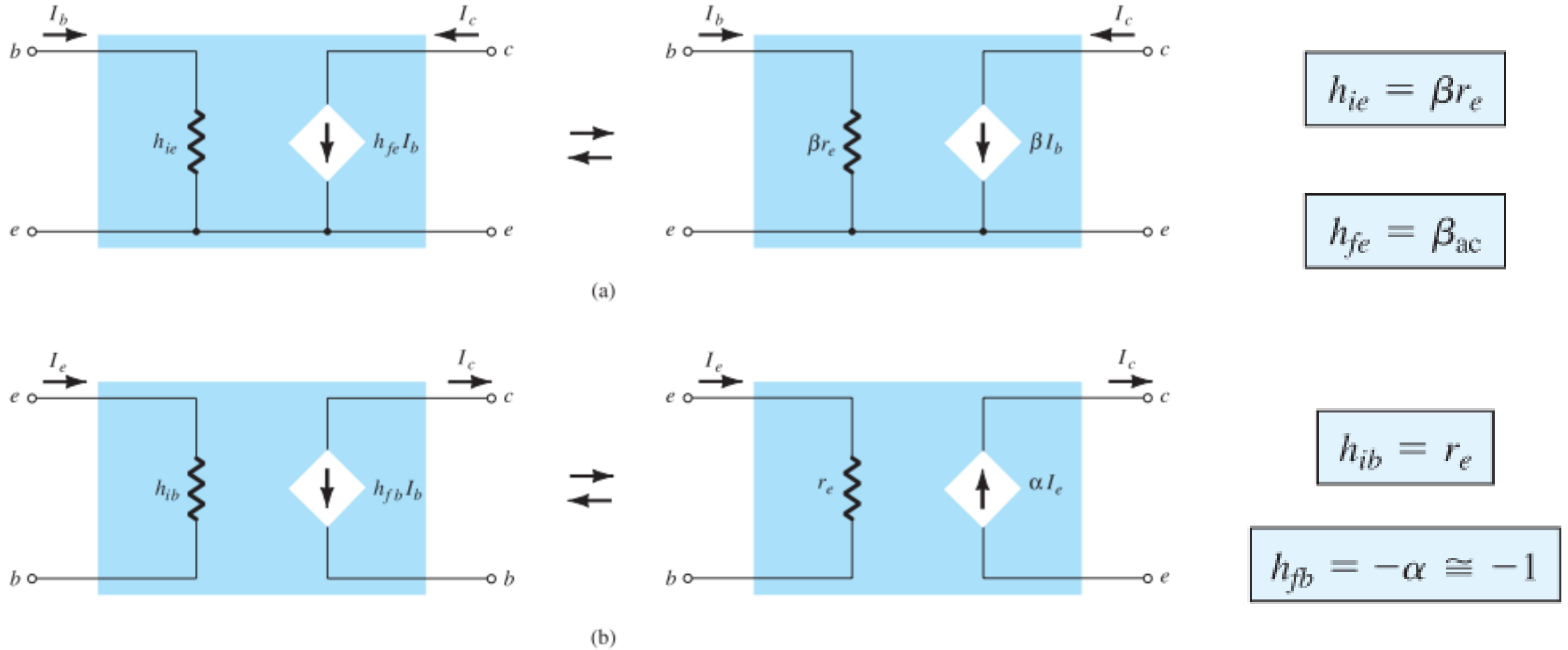


FIG. 5.101

Hybrid versus r_e model: (a) common-emitter configuration; (b) common-base configuration.

Hybrid vs. r_e model (Example)

EXAMPLE 5.19 Given $I_E = 2.5 \text{ mA}$, $h_{fe} = 140$, $h_{oe} = 20 \mu\text{S}$ (μmho), and $h_{ob} = 0.5 \mu\text{S}$, determine:

- The common-emitter hybrid equivalent circuit.
- The common-base r_e model.

Solution:

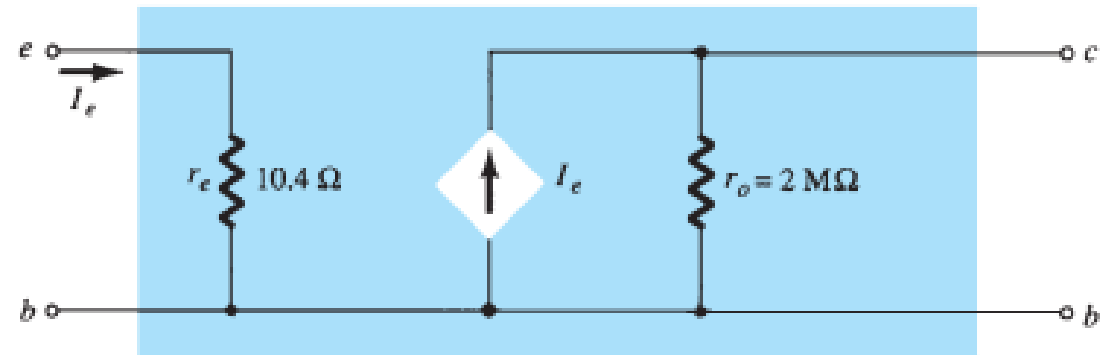
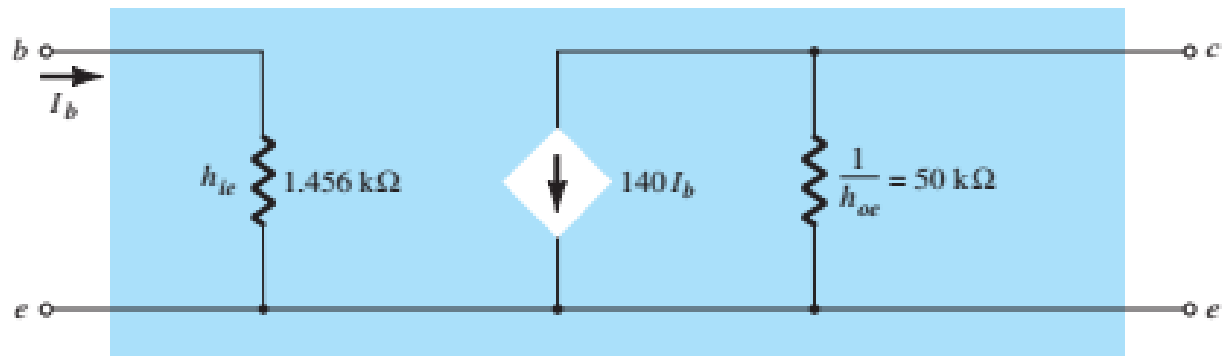
$$\text{a. } r_e = \frac{26 \text{ mV}}{I_E} = \frac{26 \text{ mV}}{2.5 \text{ mA}} = \mathbf{10.4 \Omega}$$

$$h_{ie} = \beta r_e = (140)(10.4 \Omega) = \mathbf{1.456 \text{ k}\Omega}$$

$$r_o = \frac{1}{h_{oe}} = \frac{1}{20 \mu\text{S}} = \mathbf{50 \text{ k}\Omega}$$

$$\text{b. } r_e = \mathbf{10.4 \Omega}$$

$$\alpha \cong 1, \quad r_o = \frac{1}{h_{ob}} = \frac{1}{0.5 \mu\text{S}} = \mathbf{2 \text{ M}\Omega}$$



Approximate & Complete h-model

Approximate h-model

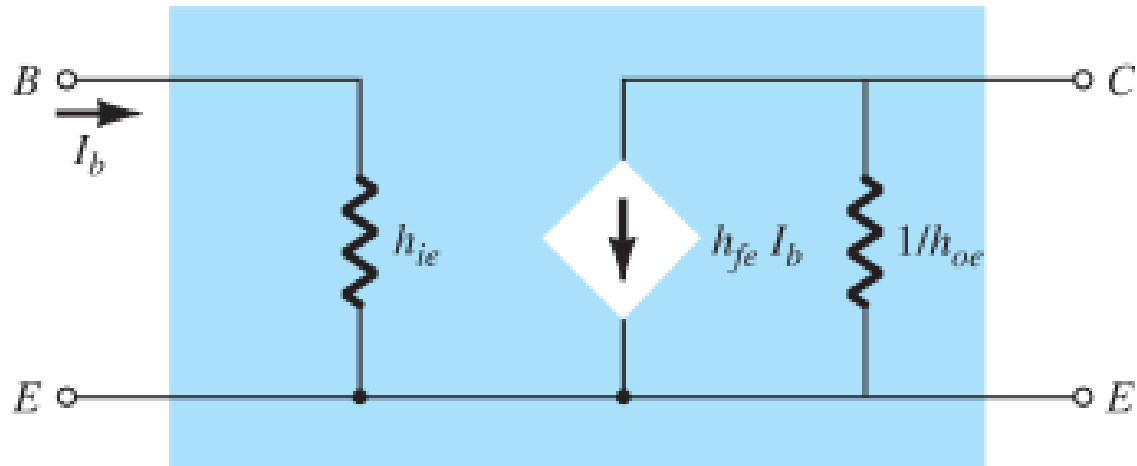


FIG. 5.104

Approximate common-emitter hybrid equivalent circuit.

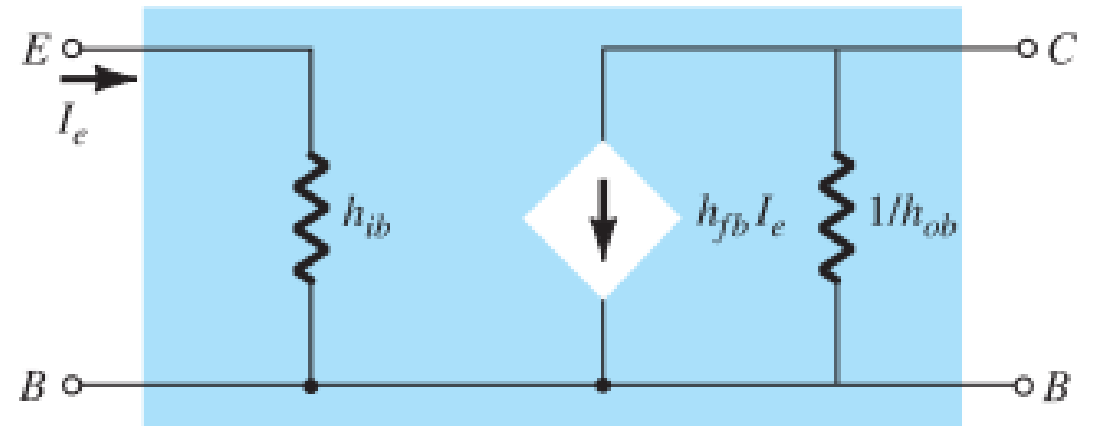
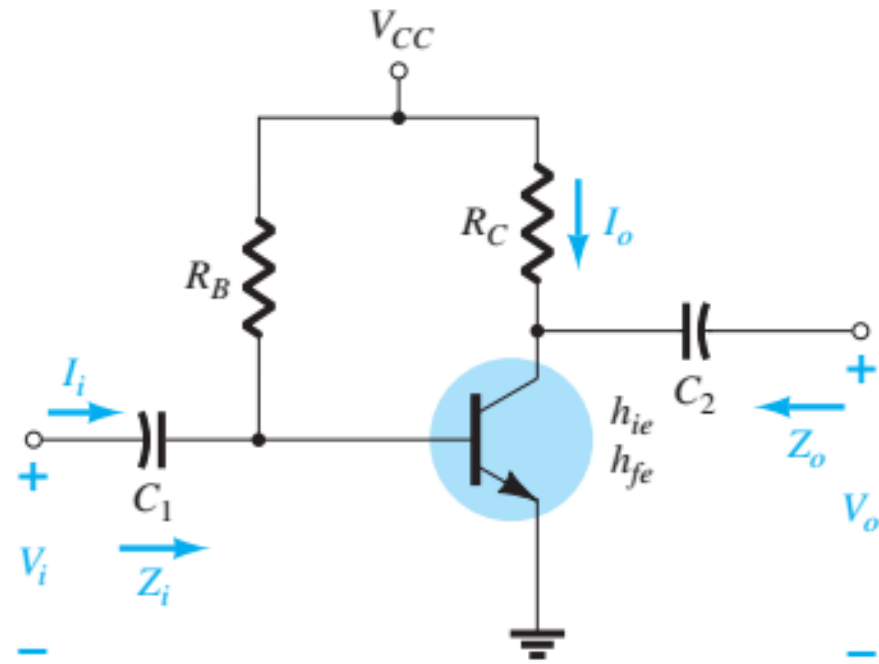


FIG. 5.105

Approximate common-base hybrid equivalent circuit.

Approximate h-model

(Fixed Bias circuit)



$$Z_i = R_B \parallel h_{ie}$$

$$Z_o = R_C \parallel 1/h_{oe}$$

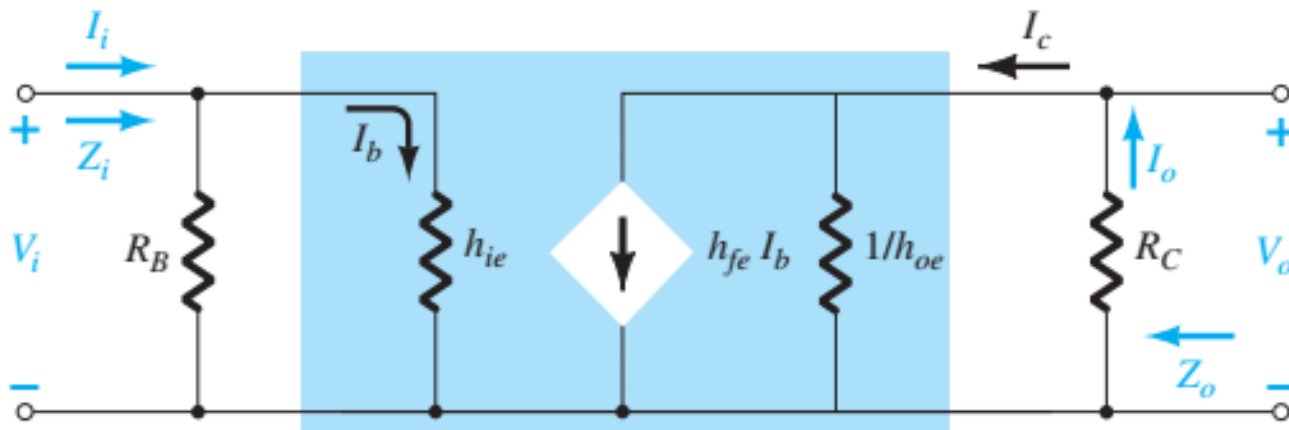
$$R' = 1/h_{oe} \parallel R_C$$

$$V_o = -I_o R' = -I_C R'$$

$$= -h_{fe} I_b R'$$

$$I_b = \frac{V_i}{h_{ie}}$$

$$V_o = -h_{fe} \frac{V_i}{h_{ie}} R'$$



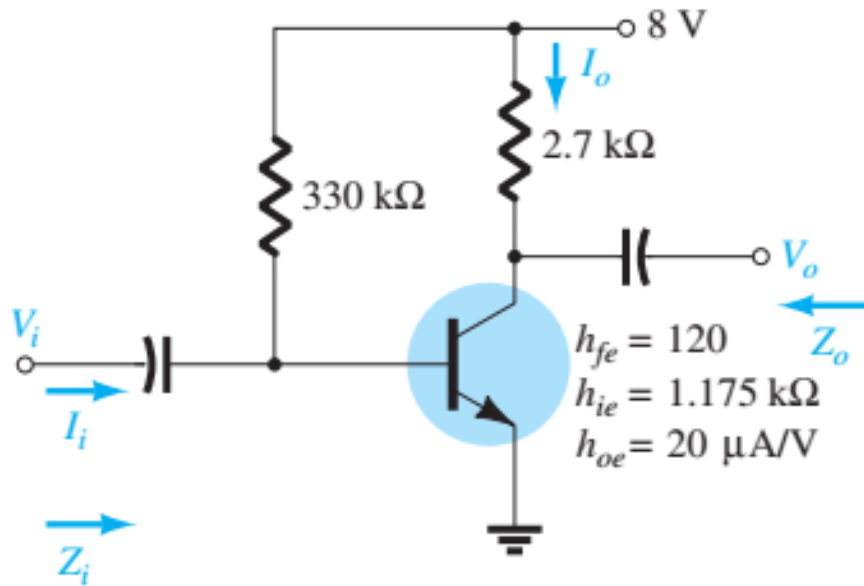
$$A_v = \frac{V_o}{V_i} = -\frac{h_{fe} (R_C \parallel 1/h_{oe})}{h_{ie}}$$

$$A_i = \frac{I_o}{I_i} \cong h_{fe}$$

Approximate h-model (Fixed Bias circuit, Example)

EXAMPLE 5.20 For the network of Fig. 5.108, determine:

- Z_i .
- Z_o .
- A_v .
- A_i .



Solution:

$$\begin{aligned} \text{a. } Z_i &= R_B \parallel h_{ie} = 330 \text{ k}\Omega \parallel 1.175 \text{ k}\Omega \\ &\cong h_{ie} = \mathbf{1.171 \text{ k}\Omega} \end{aligned}$$

$$\text{b. } r_o = \frac{1}{h_{oe}} = \frac{1}{20 \mu\text{A/V}} = 50 \text{ k}\Omega$$

$$Z_o = \frac{1}{h_{oe}} \parallel R_C = 50 \text{ k}\Omega \parallel 2.7 \text{ k}\Omega = \mathbf{2.56 \text{ k}\Omega} \cong R_C$$

$$\text{c. } A_v = -\frac{h_{fe}(R_C \parallel 1/h_{oe})}{h_{ie}} = -\frac{(120)(2.7 \text{ k}\Omega \parallel 50 \text{ k}\Omega)}{1.171 \text{ k}\Omega} = \mathbf{-262.34}$$

$$\text{d. } A_i \cong h_{fe} = \mathbf{120}$$

Check Other Configurations

Thank You!

